

Comparison between *FullSWOF\_2D*  
with a fixed time step and a fixed CFL number.  
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The purpose of this report is to compare the running of *FullSWOF\_2D* with either fixed CFL number or fixed time step.

The benchmarks used to this comparison are:

- Lake at rest with emerged bump,
- Dam break Dry without friction,
- MacDo Pseudo 2D in the long channel with subcritical flow and Manning's friction,
- MacDo Pseudo 2D in the short channel with subcritical flow and Manning's friction,
- MacDo Rain long in the channel with subcritical flow Darcy-Weisbach's friction,
- MacDo Rain long in the channel with supercritical flow Darcy-Weisbach's friction,
- MacDo on the Short channel smooth transition shock,
- Thacker planar surface in paraboloid.

## 1 Choice of time step

In this section, we describe the method to pick out the time step for the simulation with fixed time step.

In fact, I have run *FullSWOF\_2D* with the inputs of the previous benchmarks and I have chosen the time step which has the smaller value.

All simulations have been run with a CFL number equal to 0,5.

The results are plotted on the figures 1, 2, 3, 4, 5, 6.

I haven't plotted the bump and dam break's results because for these two benchmarks the time step was constant during the simulation with fixed CFL number, so I took this value of time step to run the simulation with fixed time step.

In case of Bump's simulation  $dt = 0.1s$  and dam break  $dt = 0.04s$ .

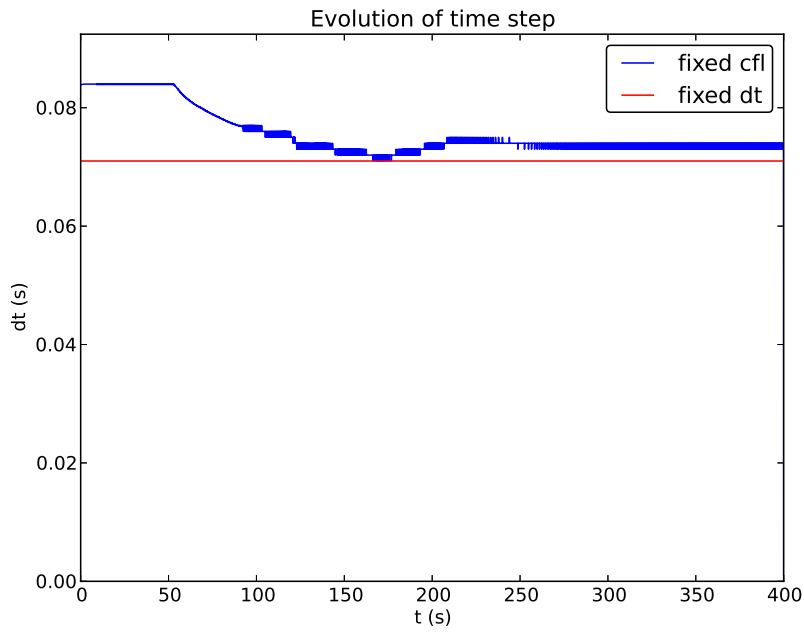


Figure 1: MacDo Pseudo 2D long channel subcritical flow Manning's friction

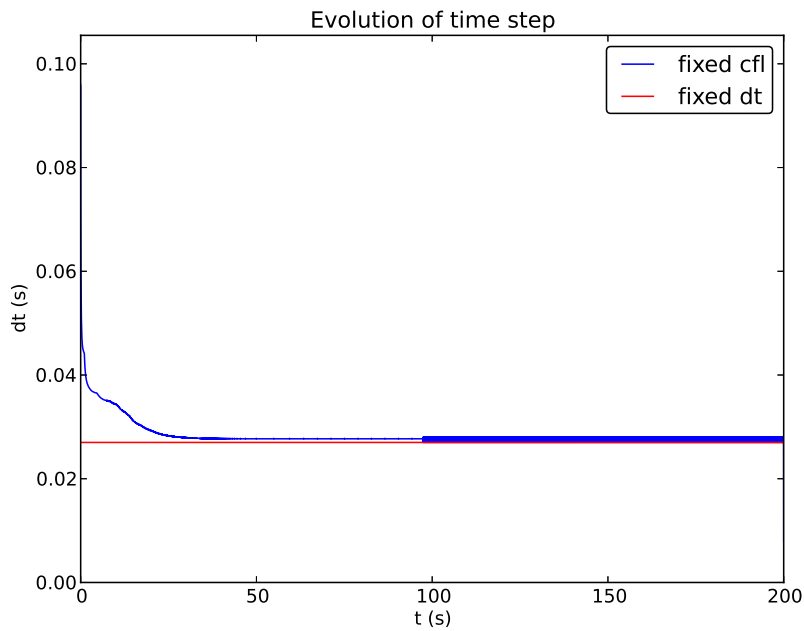


Figure 2: MacDo Pseudo 2D short channel supercritical flow Manning's friction

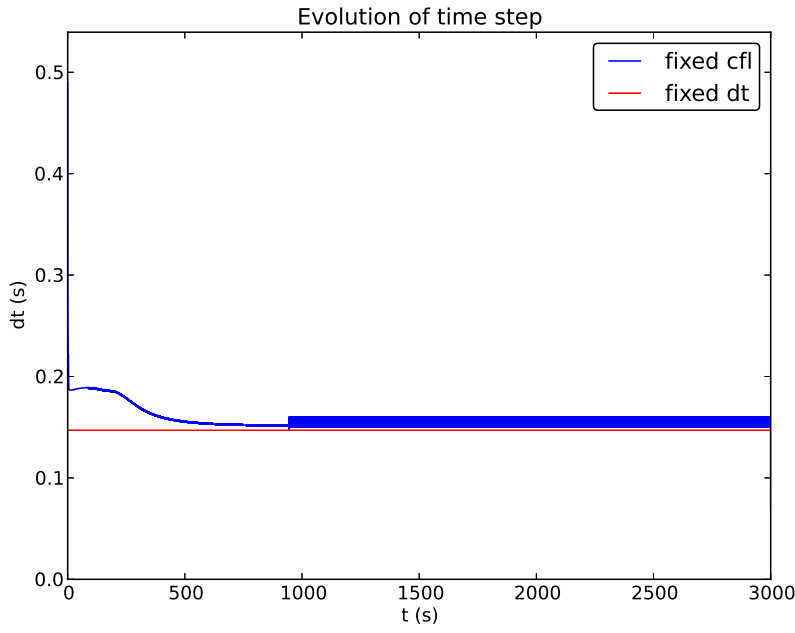


Figure 3: MacDo Rain long channel subcritical flow DW

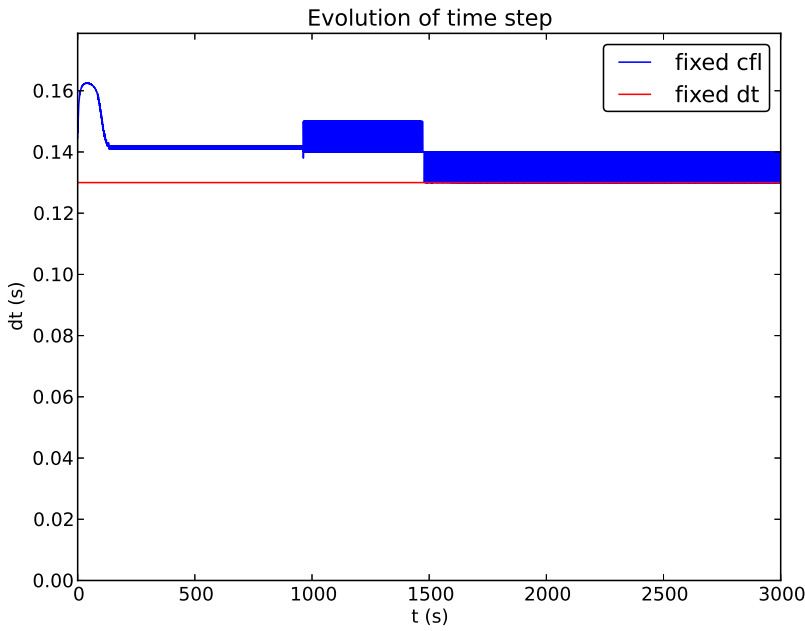


Figure 4: MacDo Rain long channel supercritical flow DW

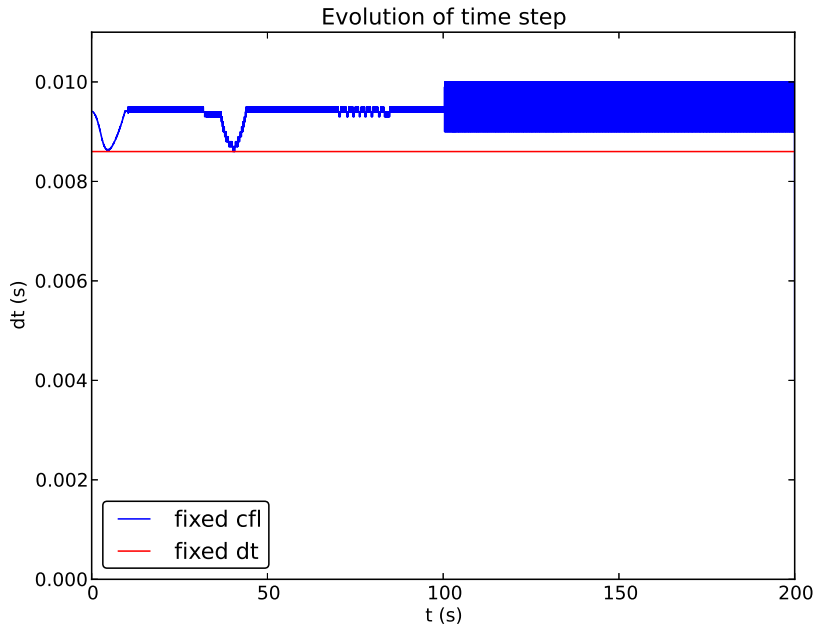


Figure 5: MacDo Short channel smooth transition shock

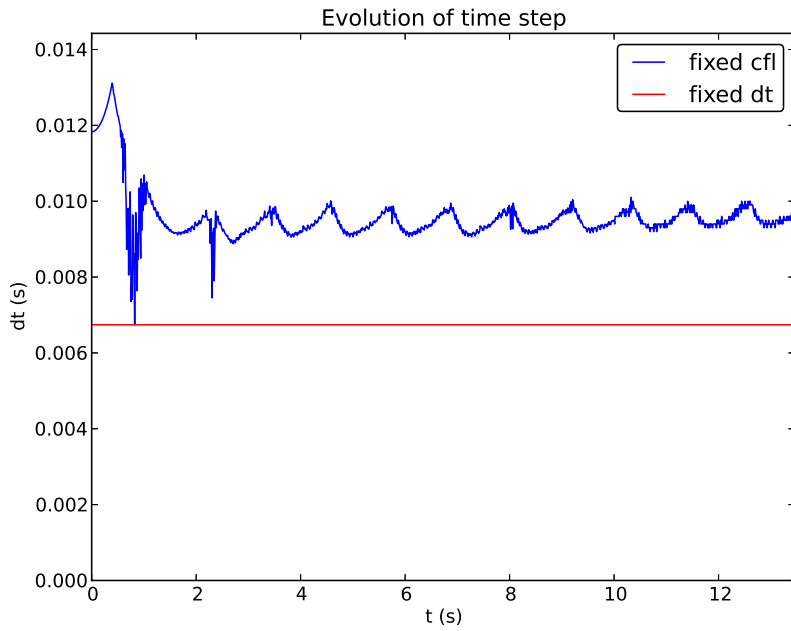


Figure 6: Thacker planar surface in paraboloid

Table 1: The Results of comparison.

	error dt/exact (%)	error cfl/exact (%)	error dt/cfl (%)	CPU time (s): dt	CPU time (s): cfl
Bump	0	0	0	24	25
Dam break	4.5	4.5	0	4	3
Pseudo 2D sub	7.8	7.8	3.e-03	86	128
Pseudo 2D sup	1.3	1.3	0	116	125
Rain sub DW	0.2	0.2	0	159	244
Rain sup DW	5.e-03	5.e-03	7.e-05	329	484
Short channel	0.4	0.4	5.e-03	110	147
Thacker	0.7	3.5	3	41	44
Total				869 ( $\approx$ 14mn)	1200 ( $\approx$ 20mn)

## 2 Numerical results

In this section, I will present the results obtained for the water height and the velocity in comparison with analytic solution.

To compare the different configurations (i.e *FullSWOF\_2D* ran with a fixed time step or fixed CFL number), I calculated two errors for each simulation with a L1's norm.

The first error (error dt/exact or error cfl/exact) is used in order to know the difference between the analytic solution and the simulation with either fixed time step or CFL's number. The calcul applied for this is:  $error = \frac{\|h_a - h\|}{\|h_a\|}$ , where  $h_a$  is the analytic solution water height and  $h$  is the water height obtained from one of both simulations.

The second error (error dt/cfl) is used to compare the difference between the two configuration. Hence, the formula applied is:  $error = \frac{\|h_{cfl} - h_{dt}\|}{\|h_{cfl}\|}$ , where  $h_{cfl}$  is the water height from simulation with CFL's number and  $h_{dt}$  is the water height from simulation with a fixed time step.

We give a table (see table 1) which sum up the results obtained for the different simulations.

Thus, as table 1 shows, the simulation with a fixed time step executes all benchmarks, with a better accuracy, more faster than the simulation with a CFL's number. The greater difference in term of accuracy is to the running of Thacker's benchmark (Figure 7). In this case, the simulation with a fixed time step is better than the simulation with a fixed CFL's number. Indeed, for this simulation the relative error is equal to 0.7% while the error is equal to 3% in case of the simulation with CFL's number.

## 3 Conclusion

The conclusion is when we run *FullSWOF\_2D* with a fixed time step, the error are smaller than *FullSWOF\_2D* with a CFL number. Moreover, *FullSWOF\_2D*

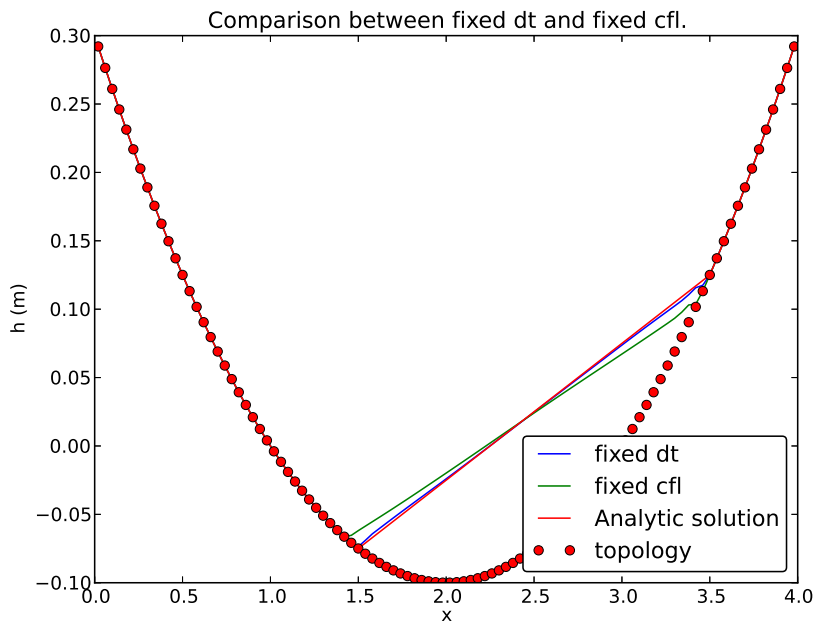


Figure 7: Thacker planar surface in paraboloid water height.

consumes less CPU time when it runs with a fixed time step.

So, if you have an assessment of the time step's value, you would take advantage of running *FullSWOF\_2D* with a fixed time step.

You can also decide to run *FullSWOF\_2D* with a CFL number to have an estimate of time step and after running it with a fixed time step.

## 4 Appendix

In this appendix, we describe the parameters of the benchmarks.

### 4.1 Lake at rest with emerged bump

#### PARAMETERS OF THE SOLUTION

Length of the domain: 25 meters

Width of the domain: 25 meters

Space step along  $x$ : 0.25 meters (Nb mailles:100)

Space step along  $y$ : 0.25 meters (Nb mailles:100)

Topography:  $z(x) = \max(0.0, 0.2 - 0.05 * (x - 10)^2)$

Solution at the steady state

Initial condition:  $h+z = 0.1$  m and  $q = 0$   $m^2/s$

Imposed discharge (left-inflow)  $q_{in} = 0$   $m^2/s$

Imposed water height (right-outflow)  $h_{out} = 0.1$  m

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Bump solution - steady state at rest with an emerged bump

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## 4.2 Short channel with smooth transition and shock

### PARAMETERS OF THE SOLUTION

Length of the domain: 100 meters

Width of the domain: 1 meters

Space step along  $x$ : 0.2 meters

Space step along  $y$ : 0.2 meters

Solution at the steady state

Initial conditions:  $h = \max(2.87871 + z(100) - z, 0)$  m and  $q = 0$   $m^2/s$

Imposed discharge on the left boundary: 2  $m^2/s$

Imposed water height on the right boundary: 2.87871m

Manning's friction coefficient: 0.0328

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MacDonald's solution - subcritical-subcritical with Manning law

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## 4.3 Rain on a long channel with subcritical flow

### PARAMETERS OF THE SOLUTION

Length of the domain: 1000 meters

Width of the domain: 10 meters

Space step along  $x$ : 2 meters

Space step along  $y$ : 2 meters

Rain intensity for  $t \geq 1500$  s: 0.001  $m/s$

Final time: 3000 s

Initial conditions:  $h = 0$  m and  $q = 0$   $m^2/s$

Imposed discharge on the left boundary for the first iteration: 1  $m^2/s$

Imposed water height on the left boundary: 0.748324 m

Imposed water height on the right boundary: 0.748324 m

Darcy-Weisbach's friction coefficient: 0.093

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MacDonald's solution - subcritical-subcritical with rain with Darcy-Weisbach law

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## 4.4 Rain on a long channel with supercritical flow

### PARAMETERS OF THE SOLUTION

Length of the domain: 1000 meters

Width of the domain: 10 meters

Space step along  $x$ : 2 meters

Space step along  $y$ : 2 meters

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Rain intensity for  $t \geq 1500$  s:  $0.001 \text{ m/s}$

Final time: 3000 s

Initial conditions:  $h = 0 \text{ m}$  and  $q = 0 \text{ m}^2/\text{s}$

Imposed discharge on the left boundary:  $2.5 \text{ m}^2/\text{s}$

Imposed water height on the left boundary:  $0.741514 \text{ m}$

Darcy-Weisbach's friction coefficient: 0.065

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MacDonald's solution - supercritical-supercritical with rain with Darcy-Weisbach law

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## 4.5 Dam break

### PARAMETERS OF THE SOLUTION

Length of the domain: 10 meters

Width of the domain: 10 meters

Position of the dam:  $x=5$  meters

Space step along x: 0.01 meter

Space step along y: 1 meter

Time value: 6 seconds

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Ritter's solution dam break on a dry soil

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## 4.6 Planar surface in a paraboloid (Thacker's solution)

### PARAMETERS OF THE SOLUTION

Length of the domain: 4 meters

Width of the domain: 4 meters

Space step in x: 0.02 meters

Space step in y: 0.02 meters

Number of cells in x: 200

Number of cells in y: 200

Topography:  $z(x) = h_0(((x - L/2)^2 + (y - l/2)^2)/a^2 - 1)$ , with  $h_0=0.1$  meters and  $a=1$  meters

Time value: 13.4571 seconds

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